## Appendix



To:

Date: March 01, 2022

From: David Schwartz, PE, PTOE

Re: Inner Loop North Transformation Study Preferred Concept Traffic Analysis

## Inner Loop North Transformation Study City of Rochester

## PREFERRED CONCEPT TRAFFIC ANALYSIS

This memo provides an update of the traffic assessment being performed as part of the Inner Loop North Transformation Study. After vetting six (6) overall concepts, including additional sub-concepts, with the City of Rochester, MCDOT, NYSDOT, GTC, technical and community advisory committees, and the public, a preferred concept was identified. The preferred concept is a refinement of Concept 6, Alternate 2: City Grid Restoration which retains a fully directional interchange with l-490 at the western limit of the study corridor (see Appendix A for plan-view sketch). This memo seeks to further assess traffic operations associated with this preferred concept while also addressing comments provided by the NYSDOT in a letter dated 11/1/21 (see Appendix B). Attached to this memo are graphics of the existing and redistributed traffic volumes at $\mathrm{I}-490$ interchanges (Appendix C) and the Genesee River crossings (Appendix D). Appendix E provides a table of the reasonable assumptions for existing daily traffic volumes and redistributed daily traffic volumes for the preferred concept. Also, attached to this memo are exported report from the HCS Analysis (Appendix F) and Synchro Analysis (Appendix G). The process for determining reasonable assumptions is summarized below:

Since the GTC's regional travel demand model utilizes a base year of 2015, a reasonable existing traffic volume was calculated by considering either the most recent pre-pandemic NYSDOT traffic count, or, if none were available, the traffic counts collected as part of this study in November 2020. These November 2020 counts were increased by a factor of $20 \%$ to account for the impacts of the Covid-19 shutdown. Reasonable redistributed traffic volumes were calculated by applying the traffic percent increase or decrease provided by the GTC's model. In some cases, the reasonable redistributed traffic volumes were manually determined. All volumes along l-490 and its ramps were balanced for the purposes of an HCS analysis.

For the intersection Level-of-Service (LOS) analysis, existing turning movement traffic volumes were obtained from the Monroe County Department of Transportation (MCDOT) Synchro models for the AM and PM peak hours. These volumes were redistributed using available AADTs from the GTC models and the available NYSDOT count program. Note that the date of the MCDOT counts were not available and NYSDOT counts were not available at all for several of the side streets. Further analysis should be conducted for all critical intersections including obtaining new traffic count data, origin-destination data for key destinations and at interchange locations, and possible consideration of additional traffic growth from future development. The intersection analysis contained below is intended to provide reasonably conservative analysis of future traffic operations of many of the critical intersections in the study area.

## Preferred Concept

The preferred concept brings the ILN corridor to grade and removes all expressway infrastructure, while providing all on and off ramp connections between the ILN corridor and I-490 in both directions. Below are summaries of some of the major volumes changes resulting from the preferred concept.

## 1. Inner Loop North Corridor

a. ILN; West of Genesee River

## i. Proposed Central Avenue (At-Grade Roadway to Replace Elevated ILN Expressway)

- Traffic is expected to decrease substantially along the ILN corridor between Plymouth Avenue and the Genesee River. The redistributed volumes along the proposed Central Avenue are likely to be approximately 16,000 to 22,000 vpd compared to its existing volume of 43,000 to $47,000 \mathrm{vpd}$. These volumes are near the upper limits of what can be supported by the proposed two-lane roadway. Providing an additional westbound through lane from State Street to the I-490 interchange ramps would improve operations at the two signals of State Street and Plymouth Avenue, as described below. (Note that NYSDOT has proposed divesture of Plymouth Avenue.)
- Replacing the ILN with an at-grade Central Avenue will create two signalized intersections at Plymouth Avenue and State Street. One of the biggest concerns for this area raised by NYSDOT was the ability to adequately process the traffic going to and from the l-490 ramps in the AM peak hour. Two alternatives were assessed. One assumed a one-lane westbound approach on Central Ave at both locations. The other removed the proposed parking lane on the northern side of Central Avenue in favor of two westbound lanes through both intersections, from Mill Street to the ramps. This would allow traffic going to l-490 to fully utilize the two receiving lanes on the west side of Plymouth Avenue. With only one westbound through lane, both intersections are expected to operate at LOS F, with delays of just over 112 seconds/vehicle at Plymouth Avenue and just over 101 seconds/vehicle delay at State Street. While these delays would occur predominately in the westbound direction during the peak 15 minutes of the peak hours, the additional time for the westbound approach would impact operations on other approaches as well. By adding a $2^{\text {nd }}$ westbound through lane, operations at both signals would be vastly improved to a LOS D with under 42 seconds of average delay/vehicle at both intersections. A more detailed analysis of the intersections with up-to-date ADTs and Turning Movement Counts should be conducted.


## b. ILN East of the Genesee River (City Grid Restoration)

i. Proposed Cumberland Street (At-Grade Roadway to Replace Depressed ILN Expressway)

- There is expected to be a $78 \%$ decrease in traffic along the proposed Cumberland Street between St. Paul Street and North Street/North Chestnut Street. The redistributed volumes will likely be 7,000 to $9,000 \mathrm{vpd}$. The proposed two-lane roadway would be able to support these volumes.


## ii. Central Avenue

- Central Avenue from St. Paul Street to N. Clinton Street is currently a one-way eastbound roadway and has very low traffic volumes, approximately 1,500 vpd. The preferred concept would convert it to a two-way two-lane roadway and add an expected $11,000 \mathrm{vpd}(733 \%$ increase) for a total of $12,500 \mathrm{vpd}$. The proposed twolane roadway would be able to support these volumes.
- Central Avenue from N. Clinton Avenue to North Street would have a redistributed volume likely between 10,000 to $11,000 \mathrm{vpd}$. The current configuration of this roadway would support this volume.


## iii. University Avenue

One of the major concerns of some members of the public was the additional traffic along University Avenue and its impact on future traffic delays. The additional traffic and the resulting delays for several key intersections were analyzed.

- With the removal of the Inner Loop and the reconnection of University Avenue near Union Street at Anderson Park, additional traffic will likely utilize University Avenue of North Chestnut Street. Approximately 5,300 vpd (113\% increase) are expected to be added to University Avenue. The new daily total will likely be 8,000 to 12,000 vpd compared to its existing volume of 4,000 to $5,000 \mathrm{vpd}$.
- To assess the impacts of this additional volume, Level-of-Service (LOS) and intersection delays were calculated more fully along University at N . Chestnut/North Street, Scio Street, and East Main Street using Synchro. Existing LOS grades at the four signalized intersections along University Avenue are shown in Figure 1. These four intersections currently perform at a LOS of $C$ or better. Expected LOS grades for the four existing signals and the new signal at University Ave/Gibbs St under the preferred concept are shown in Figure 2. It was initially assumed that all existing curb lines and lane configurations would be maintained. Under this assumption all intersections are likely to perform at an LOS of D or better, except the North St/N. Chestnut St/University Ave intersection, which is expected to operate at a borderline LOS E/F with an average vehicle delay of approximately 80 seconds. While this $\mathrm{E} / \mathrm{F}$ LOS is anticipated to only occur during the peak 15 minutes of the peak hour, intersection improvements were explored to improve operations. The addition of short right-turn lanes along the northbound and westbound approaches would likely bring the intersection to an acceptable LOS D, even under these peak traffic conditions. Currently, the lots on the northeast and southeast corners are vacant, so addition of short right-turning lanes would not require demolition or relocation of existing users. A more detailed analysis of this intersection with up-to-date ADTs and Turning Movement Counts should be conducted for this location.


Figure 1: Existing Level-of-Service (LOS) Grades at Signalized Intersections along University Avenue


Figure 2: Expected Level-of-Service (LOS) Grades at Signalized Intersections along University Avenue under the preferred concept
iv. Lyndhurst Street

Lyndhurst Street from North Street to Scio Street is currently a one-way eastbound roadway. The preferred concept would convert it to a two-way, two-lane roadway. Some members of the public expressed concern about additional volumes that may use this roadway as a result.

- After careful assessment of existing traffic and GTC models, it is anticipated that the volume along the roadway will stay approximately the same. However, it should
be noted that the traffic analysis did not consider any future growth associated with new development along Lyndhurst.
- Lyndhurst Street from Scio Street to Union Street will be maintained as a one-way roadway. This block will experience a likely decrease of 200 vpd ( $17 \%$ decrease). This can be attributed to removal of the Inner Loop on-ramp at the intersection of Lyndhurst Street and Scio Street.


## v. Union Street

When the Inner Loop East expressway was removed, much of the traffic that had previously used the expressway were redistributed to Union Street. Some stakeholders and members of NYSDOT were concerned about the potential impact of adding additional traffic along this already heavily traveled corridor. Union Street is currently a three-lane road with one lane in each direction and a center turn lane (CTL) from Howell Street to Broad Street with the CTL converting to an additional northbound lane to East Main Street.

- Between Howell Street and East Avenue, there will be a likely increase of 7,100 vpd ( $93 \%$ increase) for a total of 14,700 vpd and between East Avenue and E. Main Street, there will be a likely increase of 5,100 vpd ( $69 \%$ increase) for a total of 12,500 vpd. These volumes are at the upper limit of what this roadway could support.
- Level of Service and intersection delays were calculated at the intersection of Union Street and East Avenue. Using the best available data, the intersection is expected to operate at a borderline LOS E/F, with an average vehicle delay of just over 85 seconds. Most of the highest delays would occur during the peak 15 minutes of the PM peak hour. The most severe delays would occur along the northbound approach. However, the only NYSDOT ADT counts along Union Street nearby were north of the intersection, so volumes on the southern leg of the intersection, and by extension, the northbound approach, were difficult to accurately determine. New ADT and turning movement counts would provide a higher level of confidence in the volumes of this approach and the operations at the intersection.


## 2. Genesee River Crossings

a. Removal of vehicular traffic on the E. Broad Street bridge (Aqueduct Re-imagined project) and the preferred concept is likely to result in increases along the other Genesee River crossings. Court Street is expected to experience the largest percent increase, while I-490 is expected to experience the largest magnitude increase. While this high-level analysis suggests these crossings would likely be able to support these increases, localized improvements may be needed. The existing facilities at these crossings will need to be further evaluated to determine if the crossings and adjacent roadway sections can support these increases in their current configurations. Some of these detailed analyses will likely occur during the City's upcoming Aqueduct Re-imagined project. Please refer to Appendix D for graphics depicting the existing and expected redistributed traffic volumes at the Genesee River crossing. Also, refer to the I-490 section below for more information about the area of the expressway near the Frederick Douglass-Susan B. Anthony Memorial Bridge.
i. Driving Park Avenue: $+2,400$ vpd ( $14 \%$ increase)
ii. Smith Street/Bausch Street: $+2,500$ vpd ( $16 \%$ increase)
iii. ILN Corridor (Proposed Central Avenue): -30,800 vpd (65\% decrease)
iv. Andrews Street: $+3,100$ vpd ( $49 \%$ increase)
v. E. Main Street: $+3,600$ vpd ( $30 \%$ increase)
vi. E. Broad Street: $-8,600$ vpd ( $100 \%$ decrease)
vii. Court Street: $+4,900$ vpd ( $84 \%$ increase)
viii. I-490: $+13,600$ vpd ( $15 \%$ increase)
ix. Ford Street: +800 vpd (4\% increase)

Overall, the total number of river crossings is expected to decrease from 226,300 in the existing conditions to approximately 217,800 in the preferred concept; an overall decrease of 8,500 vpd (4\% decrease). Some of the decrease can be accounted for from existing local traffic along the I-490 and ILN interchange ramps making large U-Turns from the east side of the river to the west side and back again. Based on the location of the ramps, 1,000 vpd cross the river on the ILN WB from the east, continue to l-490 EB, and then cross back to the east side. An additional 1,000 vpd make the opposite move from I-490 WB to ILN EB. These large U-Turns will likely be greatly reduced, and possibly eliminated altogether, with the removal of the high-speed ILN. In other words, vehicles on the east side of the river who made these moves will likely stay on the east side and use the other roads in the network. These 2,000 vpd account for approximately 4,000 of the daily river crossings. The remaining $4,500 \mathrm{vpd}$ reduction of the river crossings may be the result of crossings along parallel roadways to the north and south of the study area. These movements may be further accounted for with an expanded GTC model.

## 3. I-490

a. Expressway Mainline
i. East of the ILN/I-490 interchange, the I-490 mainline volumes are likely to increase due to traffic diverting from the ILN corridor to I-490. To the West, however, the I-490 mainline volumes are likely to decrease slightly. This may be due to vehicles that formerly used the ILN to access I-490 WB diverting to other routes. Some of this is illustrated with the expected increase at the I-490 WB on-ramp from Brown Street. The remaining traffic likely uses other parallel routes, possibly to the north of the study area. These movements may be further accounted for with an expanded GTC model.
ii. A limited HCS analysis was completed for the I-490 mainline between the ILN corridor and the S. Clinton/South/Howell Interchange. This is where I-490 is expected to experience the largest percent increases. It should be noted that the traffic volumes were derived from ADT data and were not based on hourly counts during the peak hours. Furthermore, HCS calculations are high-level checks and do not consider the interactions between merge/diverge points, weave sections, and on and off-ramps. Due to the complexity of I490 in the area, further analysis should be completed as detailed in the Recommendations section below. The HCS analysis conducted illustrates what areas will likely be the most heavily impacted by the ILN removal and provides a reasonably conservative estimate of traffic operations.
iii. I-490 WB between S. Plymouth and ILN Corridor

- Basic Freeway Section
- Existing Peak Hour LOS: B
- Redistributed Peak Hour LOS: C
iv. I-490 EB between ILN Corridor and S. Plymouth
- Basic Freeway Section
- Existing Peak Hour LOS: C
- Redistributed Peak Hour LOS: C
v. I-490 WB between S. Clinton/South/Howell and S. Plymouth
- Weave Freeway Section
- Existing Peak Hour LOS: C
- Redistributed Peak Hour LOS: E
vi. I-490 EB between S. Plymouth and S. Clinton/South/Howell
- Weave Freeway Section
- Existing Peak Hour LOS: D
- Redistributed Peak Hour LOS: E

This analysis reveals that there is virtually no degradation of service expected along l-490 west of the ILN interchange ramp. The less than 1 mile stretch of I-490 between S. Plymouth and the S . Clinton/South/Howell interchange, however, will likely experience some degradation of service during the peak hours of operation. While they do not reach a failing level-of-service, they are expected to drop from LOS C and D to a concerning LOS E. Under these conditions, traffic volumes are approaching the capacity of the freeway and operations become more volatile. Speeds slow noticeably, there is little room to maneuver, vehicles entering on ramps may cause a disruption wave through the traffic stream, but traffic typically does not gridlock. As noted previously, however, these analyses are based on peak hour volumes derived from ADT volumes, not up to date hourly counts. New analysis with hourly counts, specific O-D data, and using a model that considers interactions of merge/diverge points, weave areas, and ramps should be conducted to identify and evaluate feasible l—490 mainline and/or ramp mitigation strategies.

## b. Interchange with ILN Corridor

i. The preferred concept preserves the two off-ramps from I-490 EB and WB to ILN corridor and the two on-ramps to I-490 EB and WB from ILN corridor. Since the ILN is brought to grade under this concept, there is only one ramp connecting I-490 WB from Plymouth and the ILN corridor.
ii. The off-ramp from I-490 EB to the ILN corridor is expected to experience a decrease of $5,600 \mathrm{vpd}$ ( $30 \%$ decrease) in traffic. Under the preferred concept, the existing off-ramp from I-490 EB to Cascade Drive/Allen Street is removed.
iii. The on-ramp to I-490 WB at the ILN corridor (Plymouth Avenue) is expected to experience a decrease of 9,700 vpd (50\% decrease) in traffic.
iv. The off-ramp from I-490 WB to the former ILN is expected to experience an increase of $4,600 \mathrm{vpd}$ ( $230 \%$ increase). This increase can be explained by new access opportunities being created, resulting in substantial shifts in traffic patterns. Currently, the only on and off-ramps to I-490 from local (non-ILN) streets are at the S. Plymouth interchange. The I490 WB off-ramp to Spring Street, shows a likely 2,100 vpd decrease ( $24 \%$ decrease), as these vehicles will shift to the new ILN ramp. The remaining increase likely comes from vehicles that previously used the ILN east of the Genesee River, but now will use I-490 WB to cross the river. The expected 4,600 vpd on the new ILN off-ramp should be further analyzed in detail at key locations, particularly Plymouth Avenue and possibly State Street to determine what, if any, mitigation efforts may be required.
v. The on-ramp to I-490 EB from former ILN is expected to experience an increase of 6,500 vpd (176\% increase). As with the other ramp, the increase can be explained by new access opportunities being created, resulting in substantial shifts in traffic patterns. Approximately 1,400 vpd likely shift from the on-ramp to l-490 EB from S. Plymouth Avenue. Again, the remaining increase likely comes from vehicles that previously used the ILN east of the Genesee River, but now will use I-490 EB to cross the river. These 10,200 total vehicles can likely be served by the proposed on-ramp, as a typical ramp can adequately serve up approximately 19,000 vpd.

## c. Adjacent Interchanges

i. The adjacent interchanges are expected to experience slight increases on most movements. This makes sense since the ILN corridor acts as a raceway to/from I-490 and with its removal traffic redistributes to other ramps.
ii. Brown/Broad Interchange

- $\quad+700 \mathrm{vpd}$ ( $14 \%$ increase) for I-490 WB on-ramp from W. Broad Street
- $-2,400 \mathrm{vpd}(73 \%$ decrease) for I-490 EB on-ramp from Allen Street
iii. S. Plymouth Interchange
- $-2,100$ vpd ( $24 \%$ decrease) for I-490 WB off-ramp to Spring Street
- $-1,400 \mathrm{vpd}$ ( $42 \%$ decrease) for I-490 EB on-ramp from S. Plymouth Avenue
iv. S. Clinton/South/Howell Interchange
- $+3,800 \mathrm{vpd}(60 \%$ increase) for I-490 WB on-ramp from Howell Street
- $+4,200 \mathrm{vpd}$ ( $102 \%$ increase) for I-490 EB off-ramp to Howell Street


## 4. Travel Time Comparison

A travel time analysis was performed along the ILN corridor to assess some of the impacts and efficiency of a slower, at-grade roadway with traffic signals, particularly for the movement of freight traffic to and through the area. These runs were performed during off-peak hours since most deliveries are conducted during those times. The travel runs extended from the I-490 interchange to several key destinations in the study area. Existing travel time runs were conducted along the existing ILN corridor. Future travel times were estimated based on reduced average travel speeds and added delays associated with the introduction of new signalized intersections.

The existing and future travel times and the difference between them are summarized in the table below.

| Trip | Direction |  | $\begin{array}{c}\text { Average Measured } \\ \text { Existing Off-Peak } \\ \text { Travel Time }\end{array}$ | $\begin{array}{c}\text { Average Estimated } \\ \text { Future Off-Peak Travel } \\ \text { Time }\end{array}$ |
| :---: | :---: | :---: | :---: | :---: | \(\left.\begin{array}{c}Difference between <br>

Existing \& Future\end{array}\right]\)

While the travel times under the future conditions are obviously increased, due to desired slower corridor speeds and the introduction of new signals, most of the increases are deemed to be acceptable additions. Traversing the entire corridor from the I-490 interchange to East Main Street (the current terminus of the ILN) is only expected to take approximately $41 / 2$ minutes more under the proposed route along Central and University than the existing route along the ILN expressway.

## Recommendations

As recommended by NYSDOT in their 11/1/2021 letter, the traffic analysis provided in this memo should be further refined, particularly for traffic operations at key intersections in the City Grid restoration. A full network analysis with a microsimulation tool may help to better assess the interactions of traffic throughout the system, rather than just at selected locations.

- Additional pre and post pandemic traffic data (possibly utilizing "Big Data" sources in combination with localized traffic data collection) will be required to conduct a more detailed and accurate Level-of-Service analysis for critical intersections effected by this proposed corridor transformation.
- Additional pre and post pandemic origin-destination data (possibly via "Big Data" sources) should also be obtained to further help determine traffic redistribution and more accurate future trip estimations.
- The I-490 corridor is very complex through this area with numerous lane drops, lane additions, weave areas, and merge/diverge points within a relatively short stretch. Additional data, such as peak hour count data and O-D information to better assess the impacts of the additional traffic on I-490 should be obtained (possibly utilizing "Big Data" in combination with localized traffic data collection). After obtaining this data, a more detailed analysis using a simulation model, such as VISSIM, should be conducted to fully account for all movements and traffic interactions. This assessment will help determine if feasible I-490 mainline and/or ramp mitigation measures will be necessary as part of the Inner Loop North Project.
- The GTC travel demand model should be updated to existing volumes, as indicated in NYSDOT's 11/1/2021 letter. Also indicated in the letter is that additional traffic analyses should be expanded to include other river crossings and other roadways outside of the downtown area, include additional roadways of Mount Read (Route 104) and Lake Avenue, to account for the wider impacts of the ILN removal. Ideally, it should also include Ford Street and other interchanges west and east of the study area to determine how vehicles are accessing I-490 in the absence of the ILN expressway.

APPENDIX A

APPENDIX B

November 1, 2021
Mr. Erik Frisch
Manager of Special Projects
City of Rochester DES
Architecture \& Engineering Bureau
30 Church Street, Room 300B
Rochester, NY 14614-1279
Re: Inner Loop North Transformation Planning Study
PIN 4CRO. 10

Dear Mr. Frisch,
At the October 7 Technical Advisory Committee (TAC) meeting for the Inner Loop North Transformation Study, TAC members were informed that the community's preferred concept is Concept \#6 "Restore the Grid". The primary version of Concept \#6 involves removal of the interchange ramps connecting l-490 to the western end of the Inner Loop North corridor. Two sub-concepts are also being considered, which allow the option to retain the interchange fully or partially.

NYSDOT Region 4 has reviewed materials provided by the City's prime consultant that depict Concept \#6 and its sub-concepts. While it is not possible to foresee every possible impact of this project at the current preliminary stage, we envision several traffic-related challenges on I490 mainline, adjacent interchanges, and other State-owned highways in the vicinity. We believe that mitigation may be necessary, particularly if interchange ramps are to be removed.

We offer the following comments:

1. The "heat maps" depicting changes in traffic volumes on adjacent roads resulting from diversion from the Inner Loop are based on AADT, which is somewhat deceiving. To obtain a more comprehensive understanding of the traffic impacts associated with Concept 6 and its sub-concepts, it is very important to analyze traffic diversion during the morning and evening peak hours, when many adjacent roads may already be operating near capacity. This should be done before a final concept and configuration is selected.
2. We are concerned that peak hour traffic volume increases at several locations including nearby l-490 interchange ramps and portions of l-490 mainline such as the weave section in the vicinity of the Susan B. Anthony Bridge - may be difficult to mitigate without substantial improvements. The nature of these improvements will depend upon the final Inner Loop North configuration and the above-mentioned traffic analysis.
3. The current traffic diversion analysis does not include Lake Avenue and Mount Read Boulevard, which could be impacted by the Inner Loop North Transformation. Impacts to these facilities should be analyzed and considered.
4. The GTC traffic model utilizes 2015 traffic volumes. Will the anticipated economic development along the Inner Loop North corridor generate an increase in traffic volumes? Should the traffic analysis be done using these volumes?
5. NYSDOT will propose State divesture of Plymouth Avenue under any alternative. We believe it will be more appropriate for the City of Rochester to have maintenance jurisdiction under the final configuration.

While there is potential for tremendous benefits associated with this innovative project, we are concerned about the traffic impacts Concept \#6 may have on State-owned facilities in the vicinity. We look forward to working with the City to resolve these concerns.

Sincerely,


Christopher T. Reeve, P.E.
Acting Regional Director
NYSDOT Region 4

cc: Mark J. McAnany, P.E., Principal Engineer, Bergmann Associates Joel A. Kleinberg, Acting Regional Planning \& Program Manager, NYSDOT Region 4 Paul J. Spitzer, P.E., Acting Design Engineer, NYSDOT Region 4 Matthew C. Oravec, P.E., Acting Traffic Engineer, NYSDOT Region 4 Jay R. Reisinger, P.E., Regional Local Projects Liaison, NYSDOT Region 4

APPENDIX C



APPENDIX D



APPENDIX E

|  | ROADWAY |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| I- <br> 490/BROWN/BRO AD/ALLEN INTERCHANGE | 1-490 WB; West of Interchange | 57,800 | 53,200 | -8\% |
|  | 1-490 EB; West of Interchange | 53,900 | 51,700 | -4\% |
|  | 1-490 WB; East of Interchange | 52,900 | 47,600 | -10\% |
|  | 1-490 EB; East of Interchange | 52,200 | 49,800 | -5\% |
|  | Ramp l-490 EB to Brown | 1,700 | 1,900 | 12\% |
|  | Ramp Broad to l-490 WB | 4,900 | 5,600 | 14\% |
|  | Ramp Allen to l-490 EB | 3,300 | 900 | -73\% |
| 1-490/ILN INTERCHANGE | I-490 WB; West of ILN | 52,900 | 47,600 | -10\% |
|  | 1-490 EB; West of ILN | 52,200 | 49,800 | -5\% |
|  | 1-490 WB; East of ILN | 35,600 | 44,600 | 25\% |
|  | 1-490 EB; East of ILN | 40,400 | 47,700 | 18\% |
|  | Ramp I-490 EB to ILN EB/Plymouth | 18,800 | 13,200 | -30\% |
|  | Ramp I-490 WB to ILN EB | 2,000 | 6,600 | 230\% |
|  | Ramp ILN WB/Plymouth to l-490 WB | 19,300 | 9,600 | -50\% |
|  | Ramp ILN WB to l-490 EB | 3,700 | 10,200 | 176\% |
| I-490/BOYS CLUB/S. PLYMOUTH | I-490 WB; West of Interchange | 35,600 | 44,600 | 25\% |
|  | 1-490 EB; West of Interchange | 40,400 | 47,700 | 18\% |
|  | 1-490 WB; East of Interchange | 44,300 | 51,200 | 16\% |
|  | 1-490 EB; East of Interchange | 47,700 | 54,400 | 14\% |
|  | Ramp Boys Club to I-490 EB | 4,000 | 4,800 | 20\% |
|  | Ramp S. Plymouth to I-490 EB | 3,300 | 1,900 | -42\% |
|  | Ramp I-490 WB to Spring | 8,700 | 6,600 | -24\% |
| I-490/SOUTH AVE/CLINTION INTERCHANGE | 1-490 WB; West of Interchange | 44,300 | 51,200 | 16\% |
|  | 1-490 EB; West of Interchange | 47,700 | 54,400 | 14\% |
|  | 1-490 WB; East of Interchange | 47,800 | 51,200 | 7\% |
|  | 1-490 EB; East of Interchange | 49,600 | 51,600 | 4\% |
|  | Ramp I-490 EB to South/Howell | 7,500 | 12,400 | 65\% |
|  | Ramp l-490 EB to South | 4,000 | 4,700 | 18\% |
|  | Ramp I-490 EB to Howell | 3,500 | 7,700 | 120\% |
|  | Ramp Howell to I-490 WB | 6,300 | 10,100 | 60\% |
|  | Ramp Howell to I-490 EB | 4,700 | 5,500 | 17\% |
|  | Ramp South to I-490 EB (South) | 4,500 | 4,500 | 0\% |
|  | Ramp I-490 WB to S. Clinton | 9,700 | 10,100 | 4\% |
| COMBINED ILN AND PARALLEL ROADS | Plymouth to State WB (Allen+ILN) | 21,900 | 11,300 | -48\% |
|  | Plymouth to State EB (Allen+ILN) | 21,300 | 11,100 | -48\% |
|  | Plymouth to State Combined (Allen+ILN) | 43,200 | 22,300 | -48\% |
|  | State to St. Paul (Allen+ILN) | 47,200 | 16,400 | -65\% |
|  | St. Paul to N. Clinton (Central+ILN+Cumberland) | 42,400 | 21,700 | -49\% |
|  | N. Clinton to Joseph (Central+ILN+Cumberland) | 42,000 | 19,500 | -54\% |
|  | Joseph to North (Central+ILN+Cumberland) | 40,800 | 17,800 | -56\% |
|  | North to Scio (Lyndhurst+ILN+University) | 38,200 | 10,100 | -74\% |
|  | Scio to Union (Lyndhurst+ILN+University) | 27,200 | 9,400 | -65\% |
| CITY GRID RESTORATION | St. Paul over ILN | 13,600 | 15,700 | 15\% |
|  | Central; Between St. Paul \& N. Clinton | 1,500 | 12,500 | 733\% |
|  | ILN; Between St. Paul \& N. Clinton | 41,900 | 9,200 | -78\% |
|  | Central; Between N. Clinton \& Joseph | 1,500 | 10,600 | 607\% |
|  | ILN; Between N. Clinton \& Joseph | 40,900 | 8,900 | -78\% |
|  | Central; Between Joseph \& North | 5,100 | 10,000 | 96\% |
|  | ILN; Between Joseph \& Franklin Square | 35,700 | 7,800 | -78\% |
|  | Andrews; Between Joseph \& Franklin Square | 6,200 | 6,400 | 3\% |
|  | ILN; Between Franklin Square \& North | 35,700 | 8,500 | -76\% |
|  | Andrews; Between Franklin Square \& North | 6,200 | 900 | -85\% |
|  | Lyndhurst; Between North \& Scio | 1,100 | 1,000 | -9\% |
|  | ILN; Between North \& Scio | 33,100 | 0 | -100\% |
|  | University; Between North \& Scio | 4,700 | 9,900 | 111\% |
|  | Lyndhurst; Between Scio \& Union | 1,200 | 1,000 | -17\% |
|  | University; Between Scio \& E. Main | 4,600 | 11,900 | 159\% |
| UNION STREET | Howell to East | 7,600 | 14,700 | 93\% |
|  | East to E. Main | 7,400 | 12,500 | 69\% |
| INNER LOOP RAMPS | Inner Loop WB to State | 4,300 | 0 | -100\% |
|  | State to Inner Loop EB | 5,700 | 0 | -100\% |
|  | St. Paul to Inner Loop WB | 12,500 | 0 | -100\% |
|  | Inner Loop EB to St. Paul | 8,900 | 0 | -100\% |
|  | Inner Loop WB to Joseph | 2,600 | 0 | -100\% |
|  | Joseph to Inner Loop EB | 1,700 | 0 | -100\% |
|  | Scio to Inner Loop WB | 5,700 | 0 | -100\% |
|  | Inner Loop EB to Scio | 4,800 | 0 | -100\% |
|  | E. Main to Inner Loop WB | 11,200 | 0 | -100\% |
|  | Inner Loop EB to E. Main | 9,700 | 0 | -100\% |
|  | Union to Inner Loop WB | 1,500 | 0 | -100\% |
|  | Inner Loop EB to Union | 1,600 | 0 | -100\% |


| GENESEE RIVER BRIDGE CROSSINGS | Driving Park | 17,200 | 19,600 | 14\% |
| :---: | :---: | :---: | :---: | :---: |
|  | Smith/Bausch | 15,300 | 17,800 | 16\% |
|  | Inner Loop | 47,200 | 16,400 | -65\% |
|  | Andrews | 6,300 | 9,400 | 49\% |
|  | E. Main | 12,200 | 15,800 | 30\% |
|  | E. Broad | 8,600 | 0 | -100\% |
|  | Court | 5,800 | 10,700 | 84\% |
|  | 1-490 | 92,000 | 105,600 | 15\% |
|  | Ford | 21,700 | 22,500 | 4\% |
| PERPENDICULAR ROADWAYS | Plymouth; North of ILN | 4,800 | 4,400 | -8\% |
|  | Plymouth; South of ILN | 11,400 | 9,500 | -17\% |
|  | State; North of ILN | 24,700 | 21,100 | -15\% |
|  | State; South of ILN | 17,500 | 18,700 | 7\% |
|  | St. Paul; North of ILN | 14,300 | 18,000 | 26\% |
|  | St. Paul; South of ILN | 9,000 | 9,900 | 10\% |
|  | N. Clinton; North of ILN | 10,000 | 10,900 | 9\% |
|  | N. Clinton; South of ILN | 10,900 | 9,700 | -11\% |
|  | Joseph; North of ILN | 10,600 | 11,500 | 8\% |
|  | North; North of ILN | 11,200 | 12,800 | 14\% |
|  | North; South of ILN | 12,100 | 10,200 | -16\% |
|  | Scio; North of ILN | 9,000 | 5,800 | -36\% |
|  | Scio; South of ILN | 3,800 | 4,400 | 16\% |
|  | E. Main; West of University | 9,100 | 12,000 | 32\% |
|  | E. Main; East of University | 20,200 | 17,000 | -16\% |
| AQUEDUCT | Exchange (North of Main) | 17,400 | 17,200 | -1\% |
|  | Exchange (Main to Broad) | 13,500 | 11,500 | -15\% |
|  | Exchange (Broad to Court) | 13,400 | 20,500 | 53\% |
|  | Exchange (South of Court) | 10,600 | 10,800 | 2\% |
|  | South (Main to Broad) | 8,400 | 10,400 | 24\% |
|  | South (Broad to Court) | 15,000 | 13,300 | -11\% |
|  | South (South of Court) | 15,300 | 14,800 | -3\% |
|  | Clinton (Main to Broad) | 12,100 | 12,200 | 1\% |
|  | Clinton (Broad to Court) | 14,200 | 13,100 | -8\% |
|  | Clinton (Court to Woodbury) | 17,100 | 17,200 | 1\% |
|  | Clinton (South of Woodbury) | 17,500 | 17,900 | 2\% |
|  | Main (West of Exchange) | 10,700 | 14,200 | 33\% |
|  | Main (Exchange to South) | 12,200 | 15,800 | 30\% |
|  | Main (South to Clinton) | 10,600 | 13,200 | 25\% |
|  | Broad (West of Exchange) | 7,500 | 3,400 | -55\% |
|  | Broad (Exchange to South) | 8,600 | 0 | -100\% |
|  | Broad (South to Clinton) | 7,800 | 3,700 | -53\% |
|  | Court (Exchange to South) | 5,800 | 10,900 | 88\% |
|  | Court (South to Clinton) | 6,100 | 9,200 | 51\% |
|  | Woodbury (South to Clinton) | 17,000 | 16,400 | -4\% |
|  | 1-490 WB | 44,300 | 51,200 | 16\% |
|  | 1-490 EB | 47,700 | 54,400 | 14\% |
| UNIVERSITY AVE NEIGHBORHOOD | North (North of Central) | 12,400 | 13,300 | 7\% |
|  | North (South of Central) | 16,300 | 13,500 | -17\% |
|  | Chestnut (South of University) | 11,400 | 11,800 | 4\% |
|  | Scio (North of Lyndhurst) | 9,000 | 5,900 | -34\% |
|  | Scio (Lyndhurst to Delevan) | 6,200 | 4,000 | -35\% |
|  | Scio (Delevan to University) | 3,900 | 4,000 | 3\% |
|  | Scio (South of University) | 3,800 | 3,700 | -3\% |
|  | Central (West of North) | 5,100 | 10,000 | 96\% |
|  | Lyndhurst (North to Scio) | 1,100 | 1,000 | -9\% |
|  | Lyndhurst (Scio to Union) | 1,200 | 1,000 | -17\% |
|  | University (North to Windsor) | 4,700 | 9,900 | 111\% |
|  | University (Windsor to Scio) | 4,800 | 8,200 | 71\% |
|  | University (Scio to Main) | 4,600 | 11,900 | 159\% |
|  | Andrews (West of North) | 6,200 | 900 | -85\% |
|  | E. Main; West of University | 9,100 | 12,000 | 32\% |
|  | E. Main; East of University | 20,200 | 17,000 | -16\% |

APPENDIX F

## HCS7 Basic Freeway Report

## Project Information

| Analyst | PSC | Date | $12 / 10 / 2021$ |
| :--- | :--- | :--- | :--- |
| Agency | Bergmann | Analysis Year | 2021 |
| Jurisdiction | NYSDOT | Time Period Analyzed | Existing |
| Project Description | ILN |  |  |

Geometric Data

| Number of Lanes (N), In | 3 | Terrain Type | Level |
| :--- | :--- | :--- | :--- |
| Segment Length (L), ft | - | Percent Grade, \% | - |
| Measured or Base Free-Flow Speed | Base | Grade Length, mi | - |
| Base Free-Flow Speed (BFFS), mi/h | 75.4 | Total Ramp Density (TRD), ramps $/ \mathrm{mi}$ | 4.00 |
| Lane Width, ft | 12 | Free-Flow Speed (FFS), mi/h | 65.1 |
| Right-Side Lateral Clearance, ft | 10 |  |  |

## Adjustment Factors

| Driver Population | All Familiar | Final Speed Adjustment Factor (SAF) | 1.000 |
| :--- | :--- | :--- | :--- |
| Weather Type | Non-Severe Weather | Final Capacity Adjustment Factor (CAF) | 1.000 |
| Incident Type | No Incident | Demand Adjustment Factor (DAF) | 1.000 |

## Demand and Capacity

| Volume (V), veh/h | 3151 | Heavy Vehicle Adjustment Factor (f fv ) | 0.952 |
| :--- | :--- | :--- | :--- |
| Peak Hour Factor (PHF) | 0.92 | Flow Rate (v(d), pc/h/ln | 1199 |
| Total Trucks, \% | 5.00 | Capacity (c), pc/h/ln | 2351 |
| Single-Unit Trucks (SUT), \% | - | Adjusted Capacity (Cadj), pc/h/ln | 2351 |
| Tractor-Trailers (TT), \% | Volume-to-Capacity Ratio (v/c) | 0.51 |  |
| Passenger Car Equivalent (ET) | 2.000 |  |  |

## Speed and Density

| Lane Width Adjustment (flw) | 0.0 | Average Speed (S), mi/h | 65.1 |
| :--- | :--- | :--- | :--- |
| Right-Side Lateral Clearance Adj. (frıc) | 0.0 | Density (D), pc/mi/ln | 18.4 |
| Total Ramp Density Adjustment | 10.3 | Level of Service (LOS) | C |
| Adjusted Free-Flow Speed (FFSadj), mi/h | 65.1 |  |  |

## HCS7 Basic Freeway Report

## Project Information

| Analyst | PSC | Date | $12 / 10 / 2021$ |
| :--- | :--- | :--- | :--- |
| Agency | Bergmann | Analysis Year | 2021 |
| Jurisdiction | NYSDOT | Time Period Analyzed | Redistributed |
| Project Description | ILN |  |  |

Geometric Data

| Number of Lanes (N), In | 3 | Terrain Type | Level |
| :--- | :--- | :--- | :--- |
| Segment Length (L), ft | - | Percent Grade, \% | - |
| Measured or Base Free-Flow Speed | Base | Grade Length, mi | - |
| Base Free-Flow Speed (BFFS), mi/h | 75.4 | Total Ramp Density (TRD), ramps/mi | 4.00 |
| Lane Width, ft | 12 | Free-Flow Speed (FFS), mi/h | 65.1 |
| Right-Side Lateral Clearance, ft | 10 |  |  |

## Adjustment Factors

| Driver Population | All Familiar | Final Speed Adjustment Factor (SAF) | 1.000 |
| :--- | :--- | :--- | :--- |
| Weather Type | Non-Severe Weather | Final Capacity Adjustment Factor (CAF) | 1.000 |
| Incident Type | No Incident | Demand Adjustment Factor (DAF) | 1.000 |

## Demand and Capacity

| Volume (V), veh/h | 3721 | Heavy Vehicle Adjustment Factor (f fv ) | 0.952 |
| :--- | :--- | :--- | :--- |
| Peak Hour Factor (PHF) | 0.92 | Flow Rate (v(d), pc/h/ln | 1416 |
| Total Trucks, \% | 5.00 | Capacity (c), pc/h/ln | 2351 |
| Single-Unit Trucks (SUT), \% | - | Adjusted Capacity (Cadj), pc/h/ln | 2351 |
| Tractor-Trailers (TT), \% | Volume-to-Capacity Ratio (v/c) | 0.60 |  |
| Passenger Car Equivalent (ET) | 2.000 |  |  |

## Speed and Density

| Lane Width Adjustment (fLw) | 0.0 | Average Speed (S), mi/h | 65.1 |
| :--- | :--- | :--- | :--- |
| Right-Side Lateral Clearance Adj. (frıc) | 0.0 | Density (D), pc/mi/ln | 21.8 |
| Total Ramp Density Adjustment | 10.3 | Level of Service (LOS) | C |
| Adjusted Free-Flow Speed (FFSadj), mi/h | 65.1 |  |  |

## HCS7 Basic Freeway Report

## Project Information

| Analyst | PSC | Date | $12 / 10 / 2021$ |
| :--- | :--- | :--- | :--- |
| Agency | Bergmann | Analysis Year | 2021 |
| Jurisdiction | NYSDOT | Time Period Analyzed | Existing |
| Project Description | ILN |  |  |

Geometric Data

| Number of Lanes (N), In | 3 | Terrain Type | Level |
| :--- | :--- | :--- | :--- |
| Segment Length (L), ft | - | Percent Grade, \% | - |
| Measured or Base Free-Flow Speed | Base | Grade Length, mi | - |
| Base Free-Flow Speed (BFFS), mi/h | 75.4 | Total Ramp Density (TRD), ramps $/ \mathrm{mi}$ | 4.00 |
| Lane Width, ft | 12 | Free-Flow Speed (FFS), mi/h | 65.1 |
| Right-Side Lateral Clearance, ft | 10 |  |  |

## Adjustment Factors

| Driver Population | All Familiar | Final Speed Adjustment Factor (SAF) | 1.000 |
| :--- | :--- | :--- | :--- |
| Weather Type | Non-Severe Weather | Final Capacity Adjustment Factor (CAF) | 1.000 |
| Incident Type | No Incident | Demand Adjustment Factor (DAF) | 1.000 |

## Demand and Capacity

| Volume (V), veh/h | 4497 | Heavy Vehicle Adjustment Factor (f fv ) | 0.952 |
| :--- | :--- | :--- | :--- |
| Peak Hour Factor (PHF) | 0.92 | Flow Rate (v(d), pc/h/ln | 1711 |
| Total Trucks, \% | 5.00 | Capacity (c), pc/h/ln | 2351 |
| Single-Unit Trucks (SUT), \% | - | Adjusted Capacity (Cadj), pc/h/ln | 2351 |
| Tractor-Trailers (TT), \% | Volume-to-Capacity Ratio (v/c) | 0.73 |  |
| Passenger Car Equivalent (ET) | 2.000 |  |  |

## Speed and Density

| Lane Width Adjustment (flw) | 0.0 | Average Speed (S), mi/h | 63.7 |
| :--- | :--- | :--- | :--- |
| Right-Side Lateral Clearance Adj. (frLc) | 0.0 | Density (D), pc/mi/ln | 26.9 |
| Total Ramp Density Adjustment | 10.3 | Level of Service (LOS) | D |
| Adjusted Free-Flow Speed (FFSadj), mi/h | 65.1 |  |  |

## HCS7 Basic Freeway Report

## Project Information

| Analyst | PSC | Date | $12 / 10 / 2021$ |
| :--- | :--- | :--- | :--- |
| Agency | Bergmann | Analysis Year | 2021 |
| Jurisdiction | NYSDOT | Time Period Analyzed | Redistributed |
| Project Description | ILN |  |  |

Geometric Data

| Number of Lanes (N), In | 3 | Terrain Type | Level |
| :--- | :--- | :--- | :--- |
| Segment Length (L), ft | - | Percent Grade, \% | - |
| Measured or Base Free-Flow Speed | Base | Grade Length, mi | - |
| Base Free-Flow Speed (BFFS), mi/h | 75.4 | Total Ramp Density (TRD), ramps/mi | 4.00 |
| Lane Width, ft | 12 | Free-Flow Speed (FFS), mi/h | 65.1 |
| Right-Side Lateral Clearance, ft | 10 |  |  |

## Adjustment Factors

| Driver Population | All Familiar | Final Speed Adjustment Factor (SAF) | 1.000 |
| :--- | :--- | :--- | :--- |
| Weather Type | Non-Severe Weather | Final Capacity Adjustment Factor (CAF) | 1.000 |
| Incident Type | No Incident | Demand Adjustment Factor (DAF) | 1.000 |

## Demand and Capacity

| Volume (V), veh/h | 4046 | Heavy Vehicle Adjustment Factor (f fv ) | 0.952 |
| :--- | :--- | :--- | :--- |
| Peak Hour Factor (PHF) | 0.92 | Flow Rate (v(d), pc/h/ln | 1540 |
| Total Trucks, \% | 5.00 | Capacity (c), pc/h/ln | 2351 |
| Single-Unit Trucks (SUT), \% | - | Adjusted Capacity (Cadj), pc/h/ln | 2351 |
| Tractor-Trailers (TT), \% | Volume-to-Capacity Ratio (v/c) | 0.66 |  |
| Passenger Car Equivalent (ET) | 2.000 |  |  |

## Speed and Density

| Lane Width Adjustment (flw) | 0.0 | Average Speed (S), mi/h | 64.8 |
| :--- | :--- | :--- | :--- |
| Right-Side Lateral Clearance Adj. (frıc) | 0.0 | Density (D), pc/mi/ln | 23.8 |
| Total Ramp Density Adjustment | 10.3 | Level of Service (LOS) | C |
| Adjusted Free-Flow Speed (FFSadj), mi/h | 65.1 |  |  |

## HCS7 Basic Freeway Report

## Project Information

| Analyst | PSC | Date | $12 / 10 / 2021$ |
| :--- | :--- | :--- | :--- |
| Agency | Bergmann | Analysis Year | 2021 |
| Jurisdiction | NYSDOT | Time Period Analyzed | Existing |
| Project Description | ILN |  |  |

Geometric Data

| Number of Lanes (N), In | 3 | Terrain Type | Level |
| :--- | :--- | :--- | :--- |
| Segment Length (L), ft | - | Percent Grade, \% | - |
| Measured or Base Free-Flow Speed | Base | Grade Length, mi | - |
| Base Free-Flow Speed (BFFS), mi/h | 75.4 | Total Ramp Density (TRD), ramps $/ \mathrm{mi}$ | 4.00 |
| Lane Width, ft | 12 | Free-Flow Speed (FFS), mi/h | 65.1 |
| Right-Side Lateral Clearance, ft | 10 |  |  |

## Adjustment Factors

| Driver Population | All Familiar | Final Speed Adjustment Factor (SAF) | 1.000 |
| :--- | :--- | :--- | :--- |
| Weather Type | Non-Severe Weather | Final Capacity Adjustment Factor (CAF) | 1.000 |
| Incident Type | No Incident | Demand Adjustment Factor (DAF) | 1.000 |

## Demand and Capacity

| Volume (V), veh/h | 3062 | Heavy Vehicle Adjustment Factor (f fv ) | 0.952 |
| :--- | :--- | :--- | :--- |
| Peak Hour Factor (PHF) | 0.92 | Flow Rate (v(d), pc/h/ln | 1165 |
| Total Trucks, \% | 5.00 | Capacity (c), pc/h/ln | 2351 |
| Single-Unit Trucks (SUT), \% | - | Adjusted Capacity (Cadj), pc/h/ln | 2351 |
| Tractor-Trailers (TT), \% | Volume-to-Capacity Ratio (v/c) | 0.50 |  |
| Passenger Car Equivalent (ET) | 2.000 |  |  |

## Speed and Density

| Lane Width Adjustment (flw) | 0.0 | Average Speed (S), mi/h | 65.1 |
| :--- | :--- | :--- | :--- |
| Right-Side Lateral Clearance Adj. (frıc) | 0.0 | Density (D), pc/mi/ln | 17.9 |
| Total Ramp Density Adjustment | 10.3 | Level of Service (LOS) | B |
| Adjusted Free-Flow Speed (FFSadj), mi/h | 65.1 |  |  |

## HCS7 Basic Freeway Report

## Project Information

| Analyst | PSC | Date | $12 / 10 / 2021$ |
| :--- | :--- | :--- | :--- |
| Agency | Bergmann | Analysis Year | 2021 |
| Jurisdiction | NYSDOT | Time Period Analyzed | Redistributed |
| Project Description | ILN |  |  |

Geometric Data

| Number of Lanes (N), In | 3 | Terrain Type | Level |
| :--- | :--- | :--- | :--- |
| Segment Length (L), ft | - | Percent Grade, \% | - |
| Measured or Base Free-Flow Speed | Base | Grade Length, mi | - |
| Base Free-Flow Speed (BFFS), mi/h | 75.4 | Total Ramp Density (TRD), ramps/mi | 4.00 |
| Lane Width, ft | 12 | Free-Flow Speed (FFS), mi/h | 65.1 |
| Right-Side Lateral Clearance, ft | 10 |  |  |

## Adjustment Factors

| Driver Population | All Familiar | Final Speed Adjustment Factor (SAF) | 1.000 |
| :--- | :--- | :--- | :--- |
| Weather Type | Non-Severe Weather | Final Capacity Adjustment Factor (CAF) | 1.000 |
| Incident Type | No Incident | Demand Adjustment Factor (DAF) | 1.000 |

## Demand and Capacity

| Volume (V), veh/h | 3836 | Heavy Vehicle Adjustment Factor (f fv ) | 0.952 |
| :--- | :--- | :--- | :--- |
| Peak Hour Factor (PHF) | 0.92 | Flow Rate (v(d), pc/h/ln | 1460 |
| Total Trucks, \% | 5.00 | Capacity (c), pc/h/ln | 2351 |
| Single-Unit Trucks (SUT), \% | - | Adjusted Capacity (Cadj), pc/h/ln | 2351 |
| Tractor-Trailers (TT), \% | Volume-to-Capacity Ratio (v/c) | 0.62 |  |
| Passenger Car Equivalent (ET) | 2.000 |  |  |

## Speed and Density

| Lane Width Adjustment (flw) | 0.0 | Average Speed (S), mi/h | 65.0 |
| :--- | :--- | :--- | :--- |
| Right-Side Lateral Clearance Adj. (frıc) | 0.0 | Density (D), pc/mi/ln | 22.5 |
| Total Ramp Density Adjustment | 10.3 | Level of Service (LOS) | C |
| Adjusted Free-Flow Speed (FFSadj), mi/h | 65.1 |  |  |

## HCS7 Freeway Weaving Report

## Project Information

| Analyst | PSC | Date | 12/10/2021 |
| :--- | :--- | :--- | :--- |
| Agency | Bergmann | Analysis Year | 2021 |
| Jurisdiction | NYSDOT | Time Period Analyzed | Existing |
| Project Description | ILN |  |  |

## Geometric Data

| Number of Lanes (N), In | 3 | Segment Type | Freeway |
| :--- | :--- | :--- | :--- |
| Short Length (Ls), ft | 1230 | Number of Maneuver Lanes (NwL), In | 2 |
| Weaving Configuration | One-Sided | Ramp-to-Freeway Lane Changes (LCRF), Ic | 1 |
| Terrain Type | Level | Freeway-to-Ramp Lane Changes (LCFR), Ic | 1 |
| Percent Grade, \% | - | Ramp-to-Ramp Lane Changes (LCRR), IC | 0 |
| Interchange Density (ID), int/mi | 4.00 | Cross Weaving Managed Lane | No |

## Adjustment Factors

| Driver Population | All Familiar | Final Speed Adjustment Factor (SAF) | 1.000 |
| :--- | :--- | :--- | :--- |
| Weather Type | Non-Severe Weather | Final Capacity Adjustment Factor (CAF) | 1.000 |
| Incident Type | No Incident | Demand Adjustment Factor (DAF) | 1.000 |

## Demand and Capacity

|  | FF | RF | RR | FR |
| :---: | :---: | :---: | :---: | :---: |
| Volume ( $\mathrm{V}_{\mathrm{i}}$ ), veh/h | 4021 | 242 | 81 | 654 |
| Peak Hour Factor (PHF) | 0.92 | 0.92 | 0.92 | 0.92 |
| Total Trucks, \% | 5.00 | 5.00 | 0.00 | 5.00 |
| Heavy Vehicle Adjustment Factor (f fvV ) | 0.952 | 0.952 | 1.000 | 0.952 |
| Flow Rate (vi), pc/h | 4591 | 276 | 88 | 747 |
| Weaving Flow Rate ( $\mathrm{v}_{\mathrm{w}}$ ), pc/h | 1023 | Freeway Max Capacity (cIFL), pc/h/ln |  | 2400 |
| Non-Weaving Flow Rate (vnw), pc/h | 4679 | Density-Based Capacity (ciwl), pc/h/ln |  | 2163 |
| Total Flow Rate (v), pc/h | 5702 | Demand Flow-Based Capacity (cıw), pc/h |  | 13408 |
| Volume Ratio (VR) | 0.179 | Weaving Segment Capacity (cw), veh/h |  | 6178 |
| Minimum Lane Change Rate (LCmin), Ic/h | 1023 | Adjusted Weaving Area Capacity (Cwa), veh/h |  | 6178 |
| Maximum Weaving Length (Lmax), ft | 4323 | Volume-to-Capacity Ratio (v/c) |  | 0.88 |

## Speed and Density

| Non-Weaving Vehicle Index (Inw) | 2302 | Average Weaving Speed (Sw), mi/h | 53.0 |
| :--- | :--- | :--- | :--- |
| Non-Weaving Lane Change Rate (LCNw), Ic/h | 2732 | Average Non-Weaving Speed (Snw), mi/h | 58.9 |
| Weaving Lane Change Rate (LCw), Ic/h | 1411 | Average Speed (S), mi/h | 57.7 |
| Total Lane Change Rate (LCAll), Ic/h | 4143 | Density (D), pc/mi/ln | 32.9 |
| Weaving Intensity Factor (W) | 0.589 | Level of Service (LOS) | D |

## HCS7 Freeway Weaving Report

## Project Information

| Analyst | PSC | Date | 12/10/2021 |
| :--- | :--- | :--- | :--- |
| Agency | Bergmann | Analysis Year | 2021 |
| Jurisdiction | NYSDOT | Time Period Analyzed | Redistributed |
| Project Description | ILN |  |  |

## Geometric Data

| Number of Lanes (N), In | 3 | Segment Type | Freeway |
| :--- | :--- | :--- | :--- |
| Short Length (Ls), ft | 1230 | Number of Maneuver Lanes (NwL), In | 2 |
| Weaving Configuration | One-Sided | Ramp-to-Freeway Lane Changes (LCRF), Ic | 1 |
| Terrain Type | Level | Freeway-to-Ramp Lane Changes (LCFR), Ic | 1 |
| Percent Grade, \% | - | Ramp-to-Ramp Lane Changes (LCRR), IC | 0 |
| Interchange Density (ID), int/mi | 4.00 | Cross Weaving Managed Lane | No |

## Adjustment Factors

| Driver Population | All Familiar | Final Speed Adjustment Factor (SAF) | 1.000 |
| :--- | :--- | :--- | :--- |
| Weather Type | Non-Severe Weather | Final Capacity Adjustment Factor (CAF) | 1.000 |
| Incident Type | No Incident | Demand Adjustment Factor (DAF) | 1.000 |

## Demand and Capacity

|  | FF | RF | RR | FR |
| :---: | :---: | :---: | :---: | :---: |
| Volume ( $\mathrm{V}_{\mathrm{i}}$ ), veh/h | 4177 | 125 | 61 | 1154 |
| Peak Hour Factor (PHF) | 0.92 | 0.92 | 0.92 | 0.92 |
| Total Trucks, \% | 5.00 | 5.00 | 0.00 | 5.00 |
| Heavy Vehicle Adjustment Factor (f fvV ) | 0.952 | 0.952 | 1.000 | 0.952 |
| Flow Rate (vi), pc/h | 4769 | 143 | 66 | 1318 |
| Weaving Flow Rate ( $\mathrm{v}_{\mathrm{w}}$ ), pc/h | 1461 | Freeway Max Capacity (cIFL), pc/h/ln |  | 2400 |
| Non-Weaving Flow Rate (vnw), pc/h | 4835 | Density-Based Capacity (ciwl), pc/h/ln |  | 2122 |
| Total Flow Rate (v), pc/h | 6296 | Demand Flow-Based Capacity (cıw), pc/h |  | 10345 |
| Volume Ratio (VR) | 0.232 | Weaving Segment Capacity (cw), veh/h |  | 6060 |
| Minimum Lane Change Rate (LCmin), Ic/h | 1461 | Adjusted Weaving Area Capacity (cwa), veh/h |  | 6060 |
| Maximum Weaving Length (Lmax), ft | 4866 | Volume-to-Capacity Ratio (v/c) |  | 0.99 |

## Speed and Density

| Non-Weaving Vehicle Index (Inw) | 2379 | Average Weaving Speed (Sw), mi/h | 51.8 |
| :--- | :--- | :--- | :--- |
| Non-Weaving Lane Change Rate (LCNw), Ic/h | 2767 | Average Non-Weaving Speed (SNw), mi/h | 54.8 |
| Weaving Lane Change Rate (LCw), Ic/h | 1849 | Average Speed (S), mi/h | 54.1 |
| Total Lane Change Rate (LCAll), Ic/h | 4616 | Density (D), pc/mi/ln | 38.8 |
| Weaving Intensity Factor (W) | 0.642 | Level of Service (LOS) | E |

## HCS7 Freeway Weaving Report

## Project Information

| Analyst | PSC | Date | 12/10/2021 |
| :--- | :--- | :--- | :--- |
| Agency | Bergmann | Analysis Year | 2021 |
| Jurisdiction | NYSDOT | Time Period Analyzed | Existing |
| Project Description | ILN |  |  |

## Geometric Data

| Number of Lanes (N), In | 3 | Segment Type | Freeway |
| :--- | :--- | :--- | :--- |
| Short Length (Ls), ft | 1230 | Number of Maneuver Lanes (NwL), In | 2 |
| Weaving Configuration | One-Sided | Ramp-to-Freeway Lane Changes (LCRF), IC | 1 |
| Terrain Type | Level | Freeway-to-Ramp Lane Changes (LCFR), IC | 1 |
| Percent Grade, \% | - | Ramp-to-Ramp Lane Changes (LCRR), IC | 0 |
| Interchange Density (ID), int/mi | 4.00 | Cross Weaving Managed Lane | No |

## Adjustment Factors

| Driver Population | All Familiar | Final Speed Adjustment Factor (SAF) | 1.000 |
| :--- | :--- | :--- | :--- |
| Weather Type | Non-Severe Weather | Final Capacity Adjustment Factor (CAF) | 1.000 |
| Incident Type | No Incident | Demand Adjustment Factor (DAF) | 1.000 |

## Demand and Capacity

|  | FF | RF | RR | FR |
| :---: | :---: | :---: | :---: | :---: |
| Volume ( $\mathrm{V}_{\mathrm{i}}$ ), veh/h | 3234 | 411 | 137 | 620 |
| Peak Hour Factor (PHF) | 0.92 | 0.92 | 0.92 | 0.92 |
| Total Trucks, \% | 5.00 | 5.00 | 0.00 | 5.00 |
| Heavy Vehicle Adjustment Factor (f fvV ) | 0.952 | 0.952 | 1.000 | 0.952 |
| Flow Rate (vi), pc/h | 3692 | 469 | 149 | 708 |
| Weaving Flow Rate ( $\mathrm{v}_{\mathrm{w}}$ ), pc/h | 1177 | Freeway Max Capacity (cIFL), pc/h/ln |  | 2400 |
| Non-Weaving Flow Rate (vnw), pc/h | 3841 | Density-Based Capacity (ciwl), pc/h/ln |  | 2119 |
| Total Flow Rate (v), pc/h | 5018 | Demand Flow-Based Capacity (cıw), pc/h |  | 10213 |
| Volume Ratio (VR) | 0.235 | Weaving Segment Capacity (cw), veh/h |  | 6052 |
| Minimum Lane Change Rate (LCmin), Ic/h | 1177 | Adjusted Weaving Area Capacity (cwa), veh/h |  | 6052 |
| Maximum Weaving Length (Lmax), ft | 4897 | Volume-to-Capacity Ratio (v/c) |  | 0.79 |

## Speed and Density

| Non-Weaving Vehicle Index (Inw) | 1890 | Average Weaving Speed (Sw), mi/h | 66.1 |
| :--- | :--- | :--- | :--- |
| Non-Weaving Lane Change Rate (LCNw), Ic/h | -632 | Average Non-Weaving Speed (SNw), mi/h | 58.9 |
| Weaving Lane Change Rate (LCw), Ic/h | 1565 | Average Speed (S), mi/h | 60.4 |
| Total Lane Change Rate (LCAll), Ic/h | 933 | Density (D), pc/mi/ln | 27.7 |
| Weaving Intensity Factor (W) | 0.182 | Level of Service (LOS) | C |

## HCS7 Freeway Weaving Report

## Project Information

| Analyst | PSC | Date | 12/10/2021 |
| :--- | :--- | :--- | :--- |
| Agency | Bergmann | Analysis Year | 2021 |
| Jurisdiction | NYSDOT | Time Period Analyzed | Redistributed |
| Project Description | ILN |  |  |

## Geometric Data

| Number of Lanes (N), In | 3 | Segment Type | Freeway |
| :--- | :--- | :--- | :--- |
| Short Length (Ls), ft | 1230 | Number of Maneuver Lanes (NwL), In | 2 |
| Weaving Configuration | One-Sided | Ramp-to-Freeway Lane Changes (LCRF), Ic | 1 |
| Terrain Type | Level | Freeway-to-Ramp Lane Changes (LCFR), Ic | 1 |
| Percent Grade, \% | - | Ramp-to-Ramp Lane Changes (LCRR), IC | 0 |
| Interchange Density (ID), int/mi | 4.00 | Cross Weaving Managed Lane | No |

## Adjustment Factors

| Driver Population | All Familiar | Final Speed Adjustment Factor (SAF) | 1.000 |
| :--- | :--- | :--- | :--- |
| Weather Type | Non-Severe Weather | Final Capacity Adjustment Factor (CAF) | 1.000 |
| Incident Type | No Incident | Demand Adjustment Factor (DAF) | 1.000 |

## Demand and Capacity

|  | FF | RF | RR | FR |
| :---: | :---: | :---: | :---: | :---: |
| Volume ( $\mathrm{V}_{\mathrm{i}}$ ), veh/h | 4170 | 589 | 290 | 284 |
| Peak Hour Factor (PHF) | 0.92 | 0.92 | 0.92 | 0.92 |
| Total Trucks, \% | 5.00 | 5.00 | 0.00 | 5.00 |
| Heavy Vehicle Adjustment Factor (f fvV ) | 0.952 | 0.952 | 1.000 | 0.952 |
| Flow Rate (vi), pc/h | 4761 | 672 | 315 | 324 |
| Weaving Flow Rate ( $\mathrm{v}_{\mathrm{w}}$ ), pc/h | 996 | Freeway Max Capacity (cIFL), pc/h/ln |  | 2400 |
| Non-Weaving Flow Rate (vnw), pc/h | 5076 | Density-Based Capacity (ciwl), pc/h/ln |  | 2175 |
| Total Flow Rate (v), pc/h | 6072 | Demand Flow-Based Capacity (ciw), pc/h |  | 14634 |
| Volume Ratio (VR) | 0.164 | Weaving Segment Capacity (cw), veh/h |  | 6212 |
| Minimum Lane Change Rate (LCmin), Ic/h | 996 | Adjusted Weaving Area Capacity (Cwa), veh/h |  | 6212 |
| Maximum Weaving Length (Lmax), ft | 4171 | Volume-to-Capacity Ratio (v/c) |  | 0.93 |

## Speed and Density

| Non-Weaving Vehicle Index (Inw) | 2497 | Average Weaving Speed (Sw), mi/h | 52.8 |
| :--- | :--- | :--- | :--- |
| Non-Weaving Lane Change Rate (LCNw), Ic/h | 2821 | Average Non-Weaving Speed (SNw), mi/h | 58.5 |
| Weaving Lane Change Rate (LCw), Ic/h | 1384 | Average Speed (S), mi/h | 57.5 |
| Total Lane Change Rate (LCAll), Ic/h | 4205 | Density (D), pc/mi/ln | 35.2 |
| Weaving Intensity Factor (W) | 0.596 | Level of Service (LOS) | E |

APPENDIX G




Analysis Period (min)
15
C Critical Lane Group



C Critical Lane Group



C Critical Lane Group


C Critical Lane Group

|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |


| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | 7 | 个 |  | \％ | $\uparrow$ | 「 | \％ | $\uparrow$ | 「 | \％ | F |  |
| Traffic Volume（vph） | 175 | 320 | 25 | 100 | 450 | 140 | 60 | 460 | 135 | 130 | 440 | 80 |
| Future Volume（vph） | 175 | 320 | 25 | 100 | 450 | 140 | 60 | 460 | 135 | 130 | 440 | 80 |
| Ideal Flow（vphpl） | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time（s） | 4.0 | 5.0 |  | 4.0 | 5.0 | 4.0 | 4.0 | 5.0 | 4.0 | 4.0 | 5.0 |  |
| Lane Util．Factor | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |
| Frpb，ped／bikes | 1.00 | 1.00 |  | 1.00 | 1.00 | 0.96 | 1.00 | 1.00 | 0.93 | 1.00 | 1.00 |  |
| Flpb，ped／bikes | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.99 | 1.00 |  |
| Frt | 1.00 | 0.99 |  | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 0.98 |  |
| Flt Protected | 0.95 | 1.00 |  | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |  |
| Satd．Flow（prot） | 1593 | 1658 |  | 1590 | 1676 | 1366 | 1593 | 1676 | 1321 | 1584 | 1637 |  |
| Flt Permitted | 0.14 | 1.00 |  | 0.38 | 1.00 | 1.00 | 0.19 | 1.00 | 1.00 | 0.21 | 1.00 |  |
| Satd．Flow（perm） | 234 | 1658 |  | 631 | 1676 | 1366 | 314 | 1676 | 1321 | 350 | 1637 |  |
| Peak－hour factor，PHF | 0.90 | 0.90 | 0.90 | 0.92 | 0.90 | 0.92 | 0.90 | 0.88 | 0.88 | 0.93 | 0.93 | 0.90 |
| Adj．Flow（vph） | 194 | 356 | 28 | 109 | 500 | 152 | 67 | 523 | 153 | 140 | 473 | 89 |
| RTOR Reduction（vph） | 0 | 3 | 0 | 0 | 0 | 67 | 0 | 0 | 67 | 0 | 7 | 0 |
| Lane Group Flow（vph） | 194 | 381 | 0 | 109 | 500 | 85 | 67 | 523 | 86 | 140 | 555 | 0 |
| Confl．Peds．（\＃hr） |  |  |  | 5 |  | 11 |  |  | 56 | 56 |  |  |
| Turn Type | pm＋pt | NA |  | pm＋pt | NA | pm＋ov | pm＋pt | NA | pm＋ov | pm＋pt | NA |  |
| Protected Phases | 7 | 4 |  | 3 | 8 | 1 | 5 | 2 | 3 | 1 | 6 |  |
| Permitted Phases | 4 |  |  | 8 |  | 8 | 2 |  | 2 | 6 |  |  |
| Actuated Green，G（s） | 43.7 | 34.9 |  | 36.9 | 31.5 | 35.5 | 40.9 | 37.7 | 43.1 | 42.5 | 38.5 |  |
| Effective Green，g（s） | 43.7 | 34.9 |  | 36.9 | 31.5 | 35.5 | 40.9 | 37.7 | 43.1 | 42.5 | 38.5 |  |
| Actuated g／C Ratio | 0.44 | 0.35 |  | 0.37 | 0.32 | 0.36 | 0.41 | 0.38 | 0.43 | 0.42 | 0.38 |  |
| Clearance Time（s） | 4.0 | 5.0 |  | 4.0 | 5.0 | 4.0 | 4.0 | 5.0 | 4.0 | 4.0 | 5.0 |  |
| Vehicle Extension（s） | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 3.0 | 2.0 | 3.0 | 3.0 | 2.0 |  |
| Lane Grp Cap（vph） | 221 | 578 |  | 284 | 527 | 484 | 169 | 631 | 569 | 198 | 630 |  |
| v／s Ratio Prot | c0．08 | 0.23 |  | 0.02 | c0．30 | 0.01 | 0.01 | 0.31 | 0.01 | c0．03 | c0．34 |  |
| v／s Ratio Perm | 0.30 |  |  | 0.12 |  | 0.06 | 0.15 |  | 0.06 | 0.27 |  |  |
| v／c Ratio | 0.88 | 0.66 |  | 0.38 | 0.95 | 0.18 | 0.40 | 0.83 | 0.15 | 0.71 | 0.88 |  |
| Uniform Delay，d1 | 22.1 | 27.5 |  | 21.9 | 33.5 | 22.2 | 20.9 | 28.2 | 17.3 | 25.3 | 28.6 |  |
| Progression Factor | 1.00 | 1.00 |  | 0.79 | 0.87 | 0.79 | 1.00 | 1.00 | 1.00 | 0.88 | 0.35 |  |
| Incremental Delay，d2 | 30.0 | 5.8 |  | 0.8 | 27.0 | 0.2 | 1.5 | 8.4 | 0.1 | 9.7 | 12.0 |  |
| Delay（s） | 52.1 | 33.3 |  | 18.1 | 56.2 | 17.6 | 22.4 | 36.6 | 17.4 | 32.1 | 22.0 |  |
| Level of Service | D | C |  | B | E | B | C | D | B | C | C |  |
| Approach Delay（s） |  | 39.6 |  |  | 43.0 |  |  | 31.4 |  |  | 24.0 |  |
| Approach LOS |  | D |  |  | D |  |  | C |  |  | C |  |


| Intersection Summary |  |  |  |
| :--- | ---: | :--- | ---: |
| HCM 2000 Control Delay | 34.4 | HCM 2000 Level of Service | C |
| HCM 2000 Volume to Capacity ratio | 0.91 |  | 18.0 |
| Actuated Cycle Length（s） | 100.0 | Sum of lost time（s） | E |
| Intersection Capacity Utilization | $87.0 \%$ | ICU Level of Service |  |
| Analysis Period（min） | 15 |  |  |
| C Critical Lane Group |  |  |  |


| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | * | $\uparrow$ |  | \% | $\hat{\dagger}$ |  | \% | ${ }^{1}$ |  | * | $\hat{\beta}$ |  |
| Traffic Volume (vph) | 175 | 320 | 25 | 100 | 450 | 140 | 60 | 460 | 135 | 130 | 440 | 80 |
| Future Volume (vph) | 175 | 320 | 25 | 100 | 450 | 140 | 60 | 460 | 135 | 130 | 440 | 80 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 5.0 |  | 4.0 | 5.0 |  | 4.0 | 5.0 |  | 4.0 | 5.0 |  |
| Lane Util. Factor | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  |
| Frpb, ped/bikes | 1.00 | 1.00 |  | 1.00 | 0.99 |  | 1.00 | 0.98 |  | 1.00 | 1.00 |  |
| Flpb, ped/bikes | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  |
| Frt | 1.00 | 0.99 |  | 1.00 | 0.97 |  | 1.00 | 0.97 |  | 1.00 | 0.98 |  |
| Flt Protected | 0.95 | 1.00 |  | 0.95 | 1.00 |  | 0.95 | 1.00 |  | 0.95 | 1.00 |  |
| Satd. Flow (prot) | 1593 | 1658 |  | 1590 | 1600 |  | 1593 | 1586 |  | 1593 | 1637 |  |
| Flt Permitted | 0.11 | 1.00 |  | 0.35 | 1.00 |  | 0.19 | 1.00 |  | 0.10 | 1.00 |  |
| Satd. Flow (perm) | 191 | 1658 |  | 592 | 1600 |  | 316 | 1586 |  | 174 | 1637 |  |
| Peak-hour factor, PHF | 0.90 | 0.90 | 0.90 | 0.92 | 0.90 | 0.92 | 0.90 | 0.88 | 0.88 | 0.93 | 0.93 | 0.90 |
| Adj. Flow (vph) | 194 | 356 | 28 | 109 | 500 | 152 | 67 | 523 | 153 | 140 | 473 | 89 |
| RTOR Reduction (vph) | 0 | 3 | 0 | 0 | 11 | 0 | 0 | 11 | 0 | 0 | 7 | 0 |
| Lane Group Flow (vph) | 194 | 381 | 0 | 109 | 641 | 0 | 67 | 665 | 0 | 140 | 555 | 0 |
| Confl. Peds. (\#/hr) |  |  |  | 5 |  | 11 |  |  | 56 | 56 |  |  |
| Turn Type | pm+pt | NA |  | pm+pt | NA |  | pm+pt | NA |  | pm+pt | NA |  |
| Protected Phases | 7 | , |  | 3 | 8 |  | 5 | 2 |  | 1 | 6 |  |
| Permitted Phases | 4 |  |  | 8 |  |  | 2 |  |  | 6 |  |  |
| Actuated Green, G (s) | 41.2 | 35.2 |  | 39.2 | 34.2 |  | 41.0 | 37.8 |  | 42.6 | 38.6 |  |
| Effective Green, g (s) | 41.2 | 35.2 |  | 39.2 | 34.2 |  | 41.0 | 37.8 |  | 42.6 | 38.6 |  |
| Actuated g/C Ratio | 0.41 | 0.35 |  | 0.39 | 0.34 |  | 0.41 | 0.38 |  | 0.43 | 0.39 |  |
| Clearance Time (s) | 4.0 | 5.0 |  | 4.0 | 5.0 |  | 4.0 | 5.0 |  | 4.0 | 5.0 |  |
| Vehicle Extension (s) | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 2.0 |  | 3.0 | 2.0 |  |
| Lane Grp Cap (vph) | 162 | 583 |  | 281 | 547 |  | 170 | 599 |  | 130 | 631 |  |
| v/s Ratio Prot | c0.07 | 0.23 |  | 0.02 | 0.40 |  | 0.01 | c0.42 |  | c0.04 | 0.34 |  |
| v/s Ratio Perm | c0.42 |  |  | 0.13 |  |  | 0.15 |  |  | 0.41 |  |  |
| v/c Ratio | 1.20 | 0.65 |  | 0.39 | 1.17 |  | 0.39 | 1.11 |  | 1.08 | 0.88 |  |
| Uniform Delay, d1 | 26.6 | 27.3 |  | 20.6 | 32.9 |  | 20.8 | 31.1 |  | 28.7 | 28.5 |  |
| Progression Factor | 1.00 | 1.00 |  | 0.77 | 0.89 |  | 1.00 | 1.00 |  | 1.97 | 0.38 |  |
| Incremental Delay, d2 | 133.7 | 5.6 |  | 0.8 | 94.3 |  | 1.5 | 71.0 |  | 96.1 | 11.6 |  |
| Delay (s) | 160.3 | 32.9 |  | 16.6 | 123.5 |  | 22.3 | 102.1 |  | 152.7 | 22.4 |  |
| Level of Service | F | C |  | B | F |  | C | F |  | F | C |  |
| Approach Delay (s) |  | 75.7 |  |  | 108.2 |  |  | 95.0 |  |  | 48.4 |  |
| Approach LOS |  | E |  |  | F |  |  | F |  |  | D |  |


| Intersection Summary |  |  |  |
| :--- | ---: | :--- | ---: |
| HCM 2000 Control Delay | 82.8 | HCM 2000 Level of Service | F |
| HCM 2000 Volume to Capacity ratio | 1.16 |  | 18.0 |
| Actuated Cycle Length (s) | 100.0 | Sum of lost time (s) | G |
| Intersection Capacity Utilization | $106.8 \%$ | ICU Level of Service |  |
| Analysis Period (min) | 15 |  |  |
| C Critical Lane Group |  |  |  |



C Critical Lane Group

c Critical Lane Group

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations |  | \$ |  | \% | $\hat{\beta}$ |  | \% | F |  | \% | $\hat{\dagger}$ |  |
| Traffic Volume (vph) | 25 | 515 | 10 | 35 | 570 | 170 | 15 | 125 | 70 | 135 | 125 | 5 |
| Future Volume (vph) | 25 | 515 | 10 | 35 | 570 | 170 | 15 | 125 | 70 | 135 | 125 | 5 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) |  | 6.0 |  | 6.0 | 6.0 |  | 5.0 | 6.0 |  | 5.0 | 6.0 |  |
| Lane Util. Factor |  | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  |
| Frpb, ped/bikes |  | 1.00 |  | 1.00 | 0.98 |  | 1.00 | 0.98 |  | 1.00 | 1.00 |  |
| Flpb, ped/bikes |  | 1.00 |  | 0.99 | 1.00 |  | 0.99 | 1.00 |  | 1.00 | 1.00 |  |
| Frt |  | 1.00 |  | 1.00 | 0.97 |  | 1.00 | 0.95 |  | 1.00 | 0.99 |  |
| Flt Protected |  | 1.00 |  | 0.95 | 1.00 |  | 0.95 | 1.00 |  | 0.95 | 1.00 |  |
| Satd. Flow (prot) |  | 1852 |  | 1754 | 1769 |  | 1755 | 1736 |  | 1762 | 1850 |  |
| Flt Permitted |  | 0.77 |  | 0.35 | 1.00 |  | 0.65 | 1.00 |  | 0.35 | 1.00 |  |
| Satd. Flow (perm) |  | 1422 |  | 642 | 1769 |  | 1205 | 1736 |  | 658 | 1850 |  |
| Peak-hour factor, PHF | 0.81 | 0.81 | 0.81 | 0.92 | 0.92 | 0.92 | 0.87 | 0.87 | 0.87 | 0.78 | 0.78 | 0.78 |
| Adj. Flow (vph) | 31 | 636 | 12 | 38 | 620 | 185 | 17 | 144 | 80 | 173 | 160 | 6 |
| RTOR Reduction (vph) | 0 | 0 | 0 | 0 | 11 | 0 | 0 | 21 | 0 | 0 | 1 | 0 |
| Lane Group Flow (vph) | 0 | 679 | 0 | 38 | 794 | 0 | 17 | 203 | 0 | 173 | 165 | 0 |
| Confl. Peds. (\#hr) | 23 |  | 14 | 14 |  | 23 | 7 |  | 10 | 10 |  | 7 |
| Turn Type | Perm | NA |  | Perm | NA |  | pm+pt | NA |  | pm+pt | NA |  |
| Protected Phases |  | 4 |  |  | 8 |  | 5 | 2 |  | 1 | 6 |  |
| Permitted Phases | 4 |  |  | 8 |  |  | 2 |  |  | 6 |  |  |
| Actuated Green, G (s) |  | 55.4 |  | 55.4 | 55.4 |  | 20.7 | 19.5 |  | 32.6 | 26.4 |  |
| Effective Green, g (s) |  | 55.4 |  | 55.4 | 55.4 |  | 20.7 | 19.5 |  | 32.6 | 26.4 |  |
| Actuated g/C Ratio |  | 0.55 |  | 0.55 | 0.55 |  | 0.21 | 0.20 |  | 0.33 | 0.26 |  |
| Clearance Time (s) |  | 6.0 |  | 6.0 | 6.0 |  | 5.0 | 6.0 |  | 5.0 | 6.0 |  |
| Vehicle Extension (s) |  | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 |  |
| Lane Grp Cap (vph) |  | 787 |  | 355 | 980 |  | 256 | 338 |  | 303 | 488 |  |
| v/s Ratio Prot |  |  |  |  | 0.45 |  | 0.00 | 0.12 |  | c0.05 | 0.09 |  |
| v/s Ratio Perm |  | c0.48 |  | 0.06 |  |  | 0.01 |  |  | c0.14 |  |  |
| v/c Ratio |  | 0.86 |  | 0.11 | 0.81 |  | 0.07 | 0.60 |  | 0.57 | 0.34 |  |
| Uniform Delay, d1 |  | 19.0 |  | 10.6 | 18.1 |  | 31.7 | 36.7 |  | 25.8 | 29.7 |  |
| Progression Factor |  | 0.61 |  | 1.09 | 1.10 |  | 0.76 | 0.86 |  | 1.00 | 1.00 |  |
| Incremental Delay, d2 |  | 11.5 |  | 0.6 | 7.2 |  | 0.1 | 2.9 |  | 2.6 | 0.4 |  |
| Delay (s) |  | 23.1 |  | 12.2 | 27.1 |  | 24.4 | 34.3 |  | 28.4 | 30.1 |  |
| Level of Service |  | C |  | B | C |  | C | C |  | C | C |  |
| Approach Delay (s) |  | 23.1 |  |  | 26.4 |  |  | 33.6 |  |  | 29.3 |  |
| Approach LOS |  | C |  |  | C |  |  | C |  |  | C |  |


| Intersection Summary |  |  |  |
| :--- | ---: | :--- | ---: |
| HCM 2000 Control Delay | 26.6 | HCM 2000 Level of Service | C |
| HCM 2000 Volume to Capacity ratio | 0.79 |  | 17.0 |
| Actuated Cycle Length (s) | 100.0 | Sum of lost time (s) | E |
| Intersection Capacity Utilization | $83.0 \%$ | ICU Level of Service |  |
| Analysis Period (min) | 15 |  |  |
| C Critical Lane Group |  |  |  |



